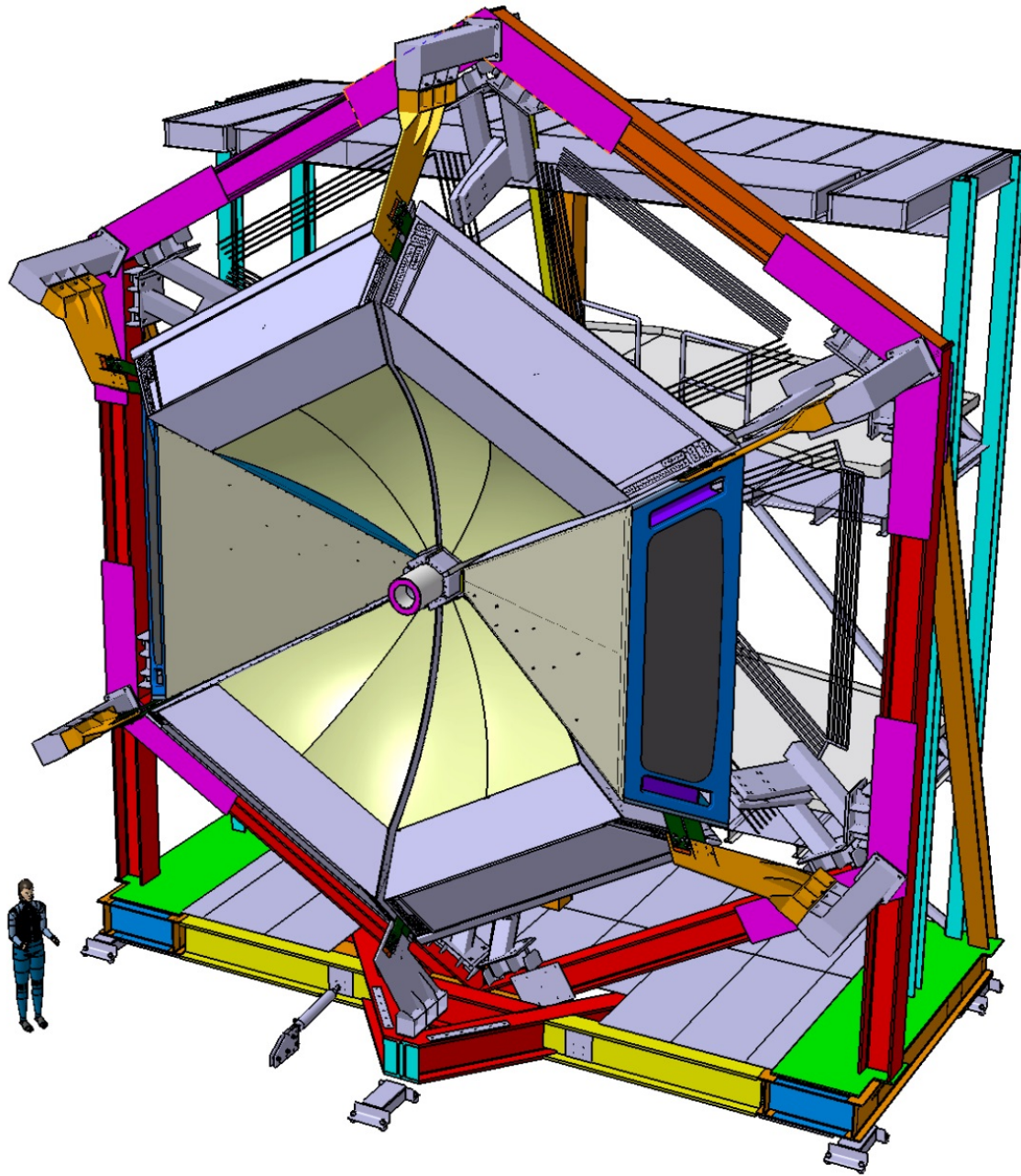


CLAS12-RICH Status-Report

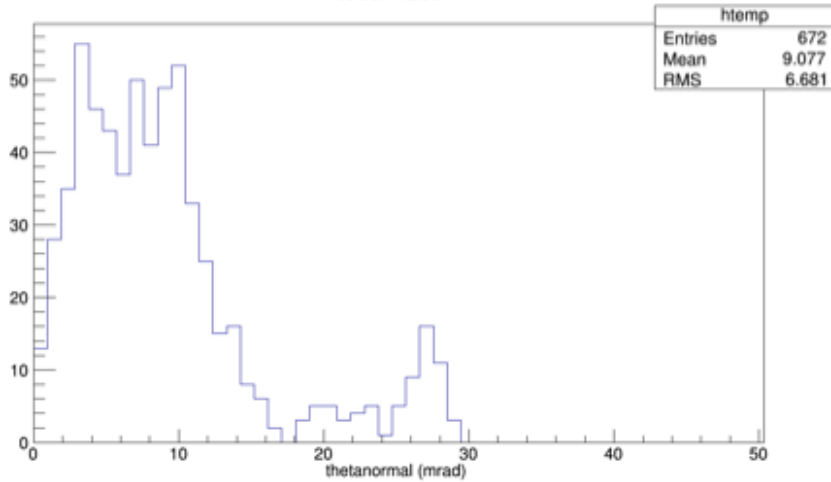
March 6th 2015



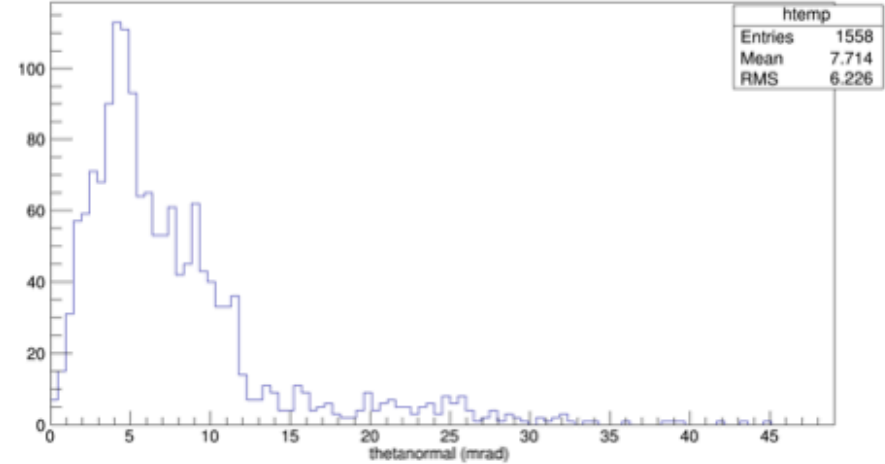
Aerogel Surface Quality

Normal angle distribution

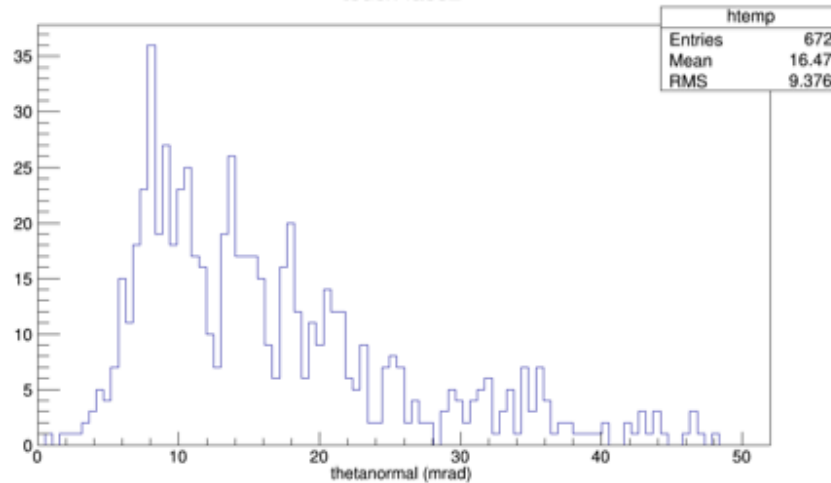
touch face1



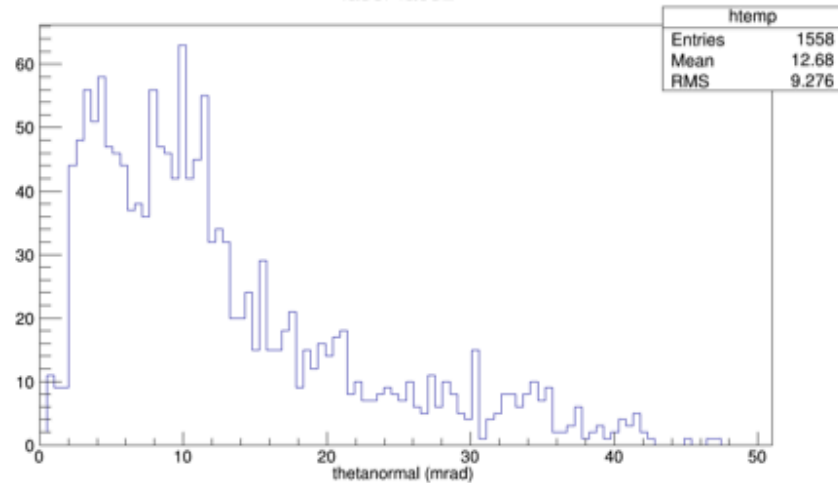
laser face1



touch face2



laser face2



Light Transmittance

Perfect aerogel surface ($n = n_{\text{Aero}}/n_{\text{Air}} \sim 1.05$)

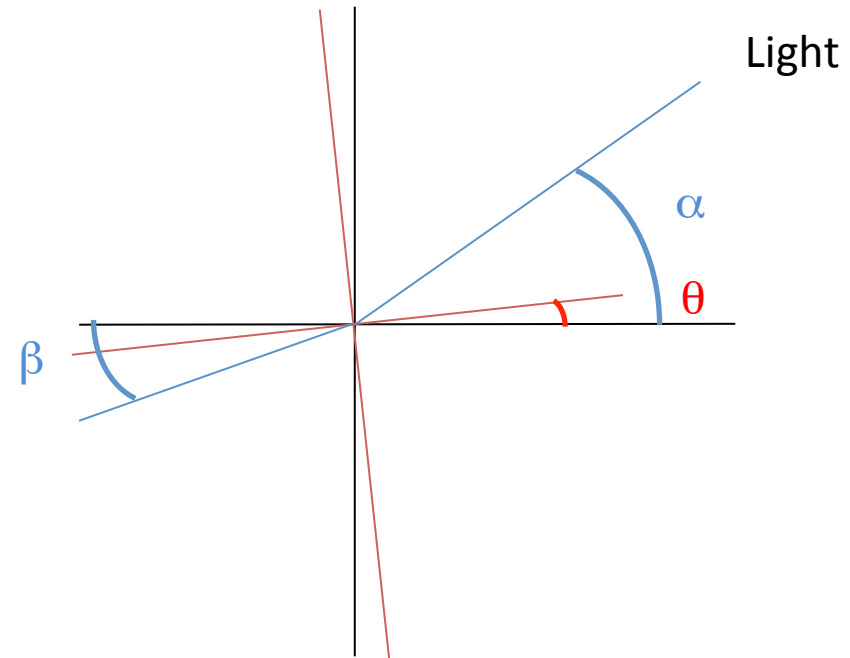
$$\beta = \text{asin}(1/n \sin \alpha)$$

Aerogel surface with normal error θ

$$\beta = \theta + \text{asin}(1/n \sin(\alpha - \theta))$$

Surface transmittance angular spread

$$\sigma \sim (1 - 1/n) \sigma_{\theta} \sim 0.05 \sigma_{\theta}$$



Aerogel transmittance angular error ($\alpha_e = \alpha_i$ if $\theta_e = \theta_i$)

$$\alpha_e = \theta_e + \text{asin}(n \sin(\beta - \theta_e)) =$$

$$= \theta_e + \text{asin}(n \sin(\theta_i - \theta_e + \text{asin}(1/n \sin(\alpha_i - \theta_i)))) \sim \alpha_i + 0.05(\theta_i - \theta_e)$$

Aerogel transmittance angular spread for independent surface errors

$$\sigma = (n - 1) \sqrt{2} \sigma_{\theta} \sim 0.05 \sqrt{2} \sigma_{\theta}$$

Angular spread due to aerogel surface (double pass)

$$\sigma \sim 0.1 \sigma_{\theta}$$

Light Reflection

Perfect mirror surface

$$\beta = \alpha$$

Mirror surface with normal error θ

$$\beta = \alpha - 2\theta$$

Surface reflection angular spread

$$\sigma \sim 2\sigma_\theta$$

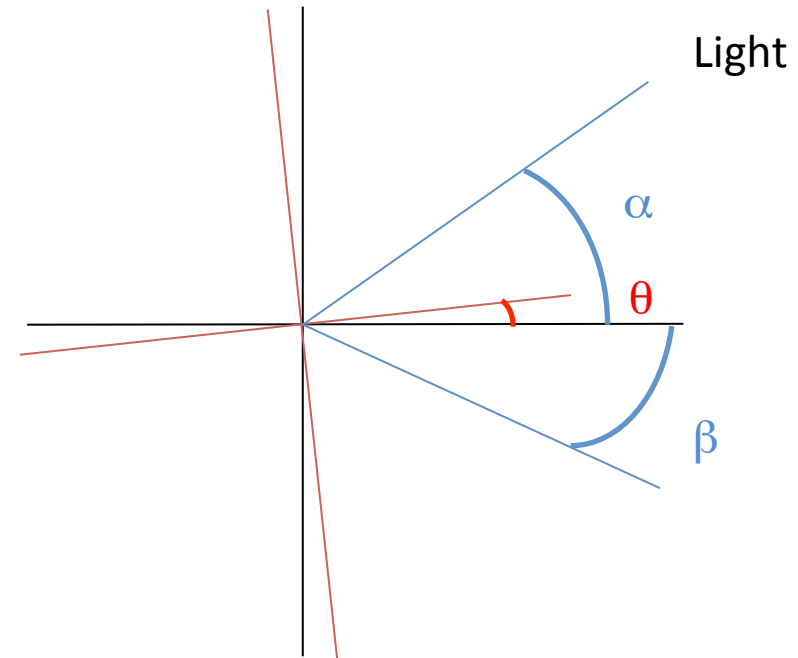
Photon detector 2D resolution

$$\sigma_x \sim \sqrt{2} / \sqrt{12} \times 6 \text{ mm} \sim 2.45 \text{ mm}$$

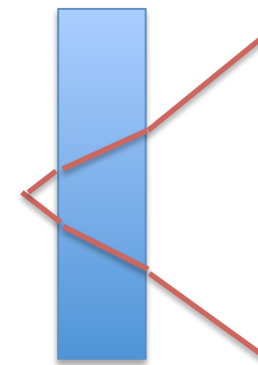
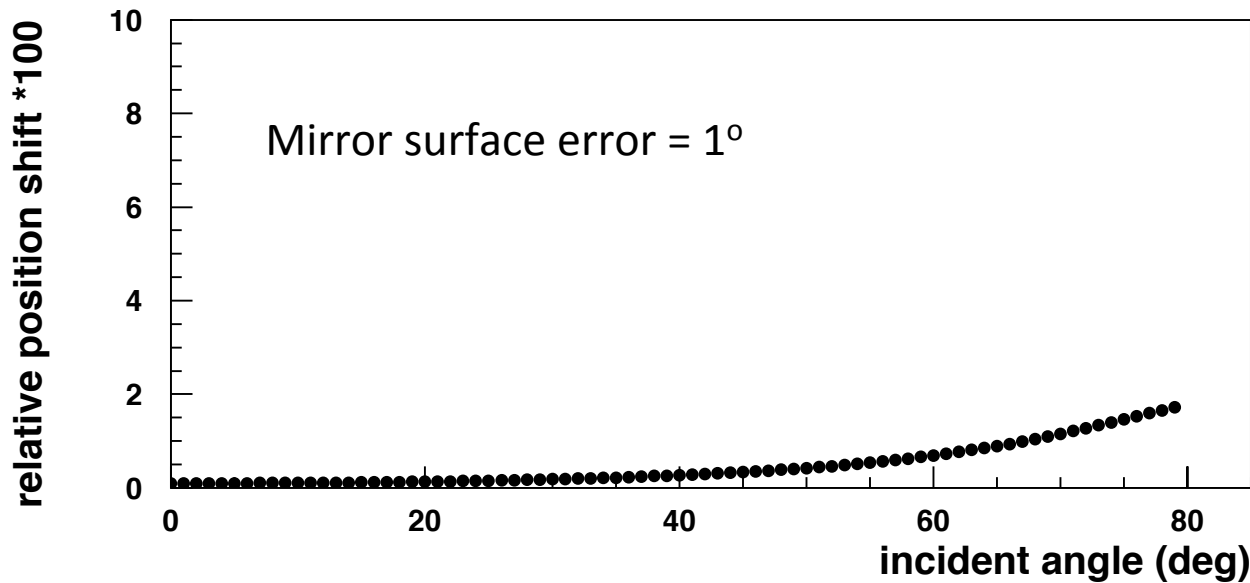
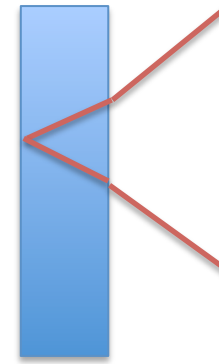
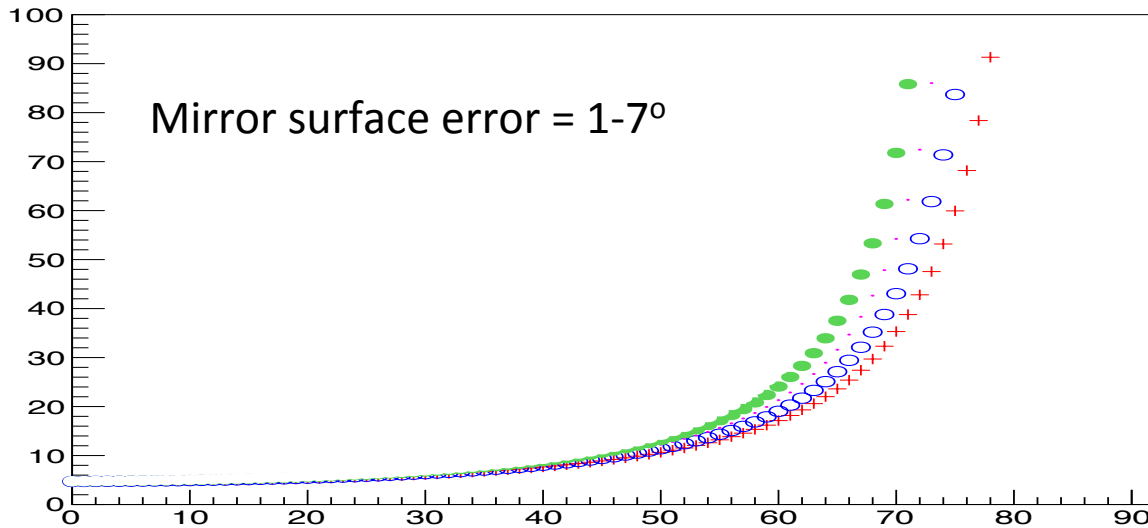
Acceptable surface error spread at distance $L = 1000 \text{ mm}$

Planar mirror: $\sigma = \sigma_x / 2 L = 1.2 \text{ mrad}$

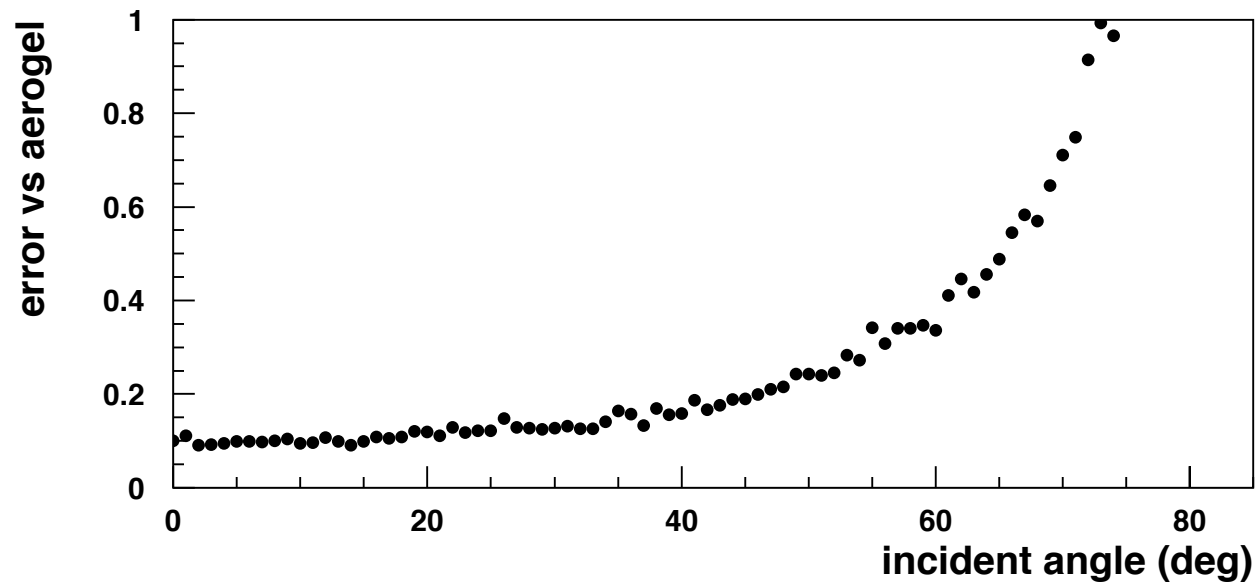
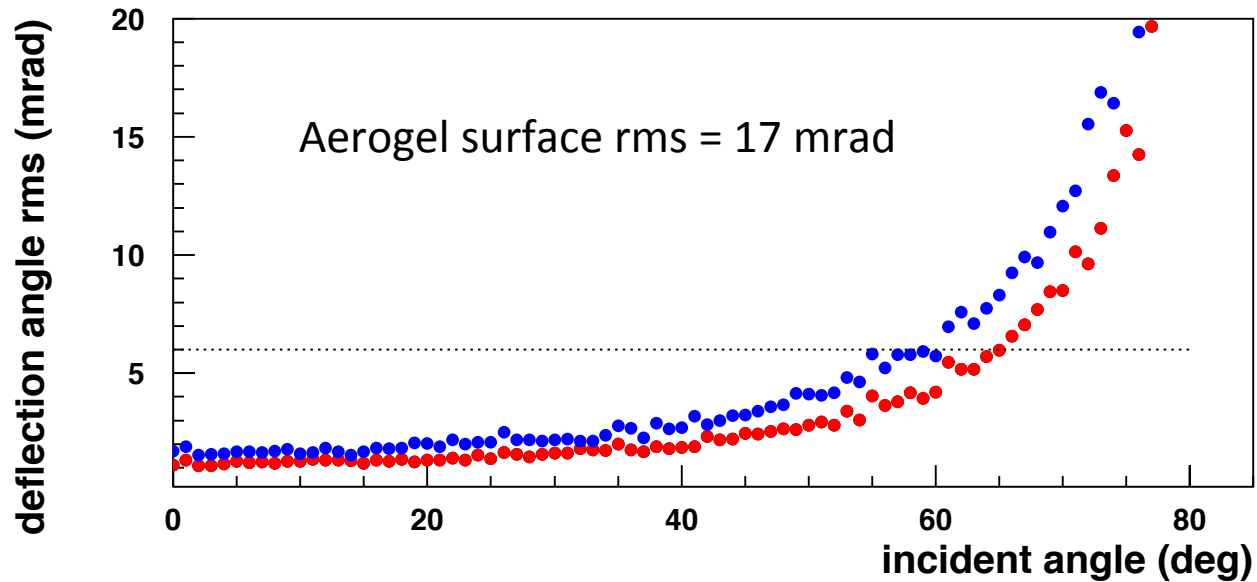
Aerogel: $\sigma = \sigma_x / 0.05 L = 49 \text{ mrad}$



Planar Mirror Surface Quality



Aerogel Surface Quality



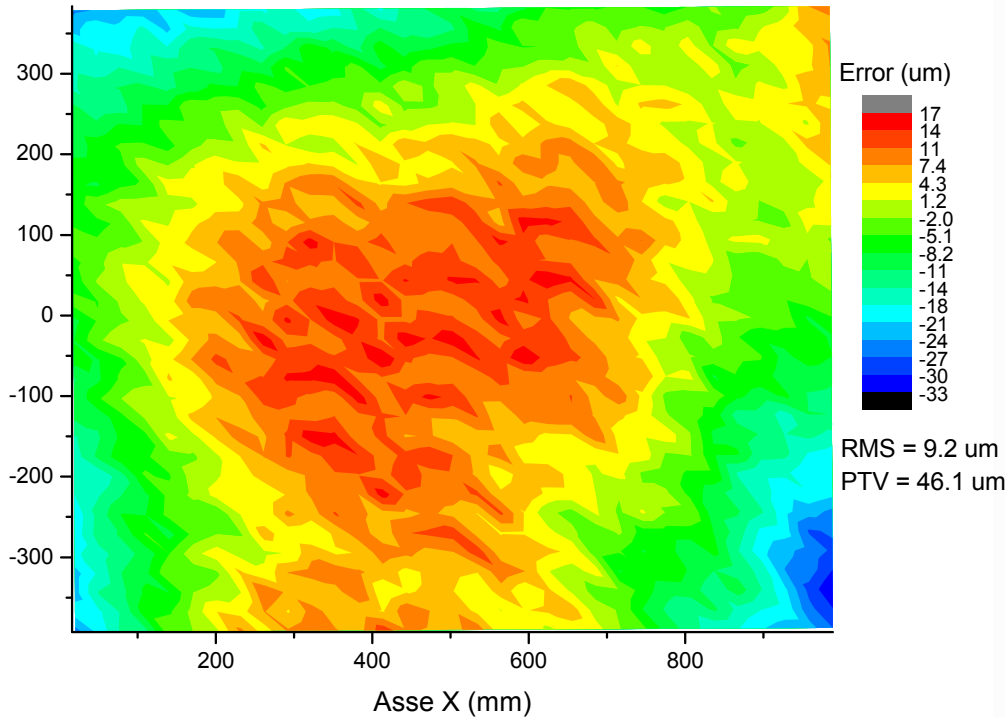
Media-Lario Mirror

Peak-to-valley similar to the mandrel
but σ_θ is acceptable:

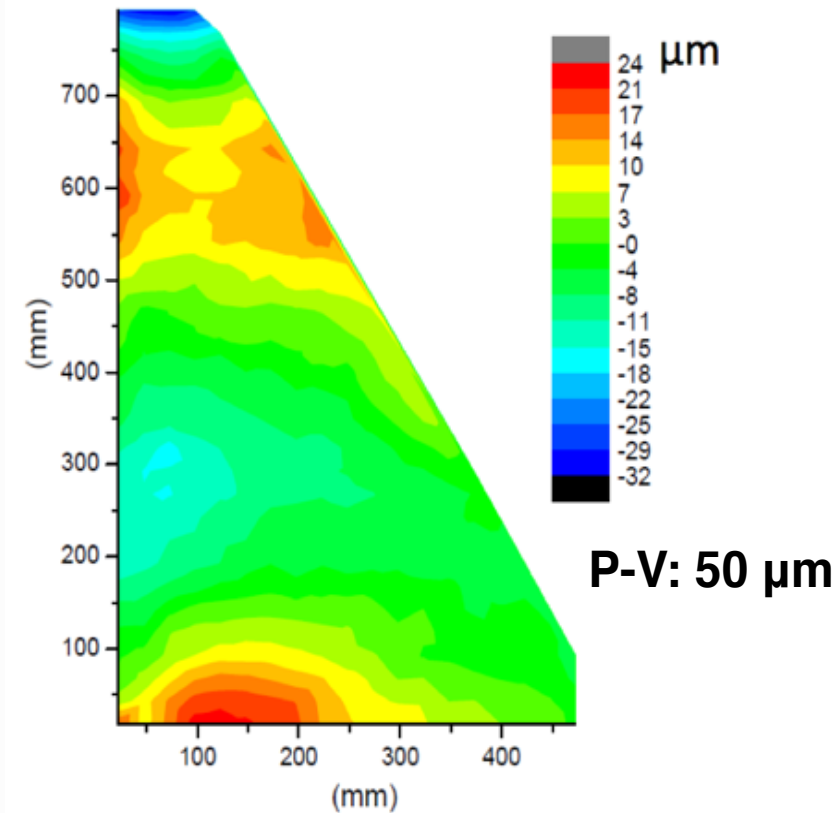
$$\sigma_\theta = 0.1 \text{ mrad}$$

do we need to improve the mandrel ?

Master - RICH - Measurement 06/03/2014



P-V: 46 μm



Glass Mirror Optimization

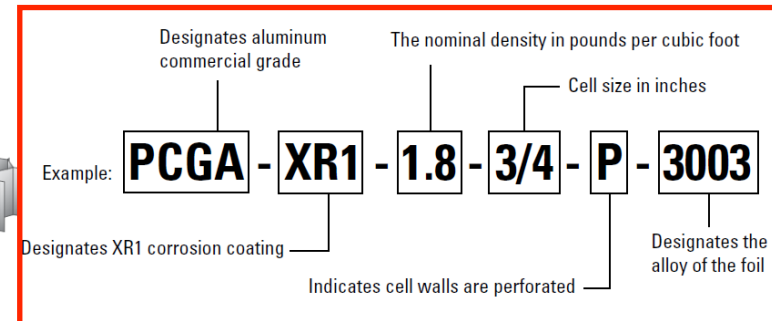
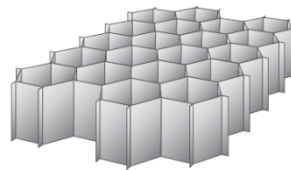
For the future production four type of optimizations are foreseen:

1. Reduction of the glass thickness from 1.6 mm to 0.7 mm per each skin and density (2200 instead of 2500 kg/m³)
2. Usage of a lighter honeycomb aluminum core (49,65 kg/m³ instead 83,3 kg/m³) with a smaller cell (1/8" instead of 1/4"). The new weight is 1.7 kg instead 2.8 kg.
3. Relocation of the foot positions

The weight gain (due to #1 and #2) is **1.1 kg** (1.7 kg instead 2.8 kg)

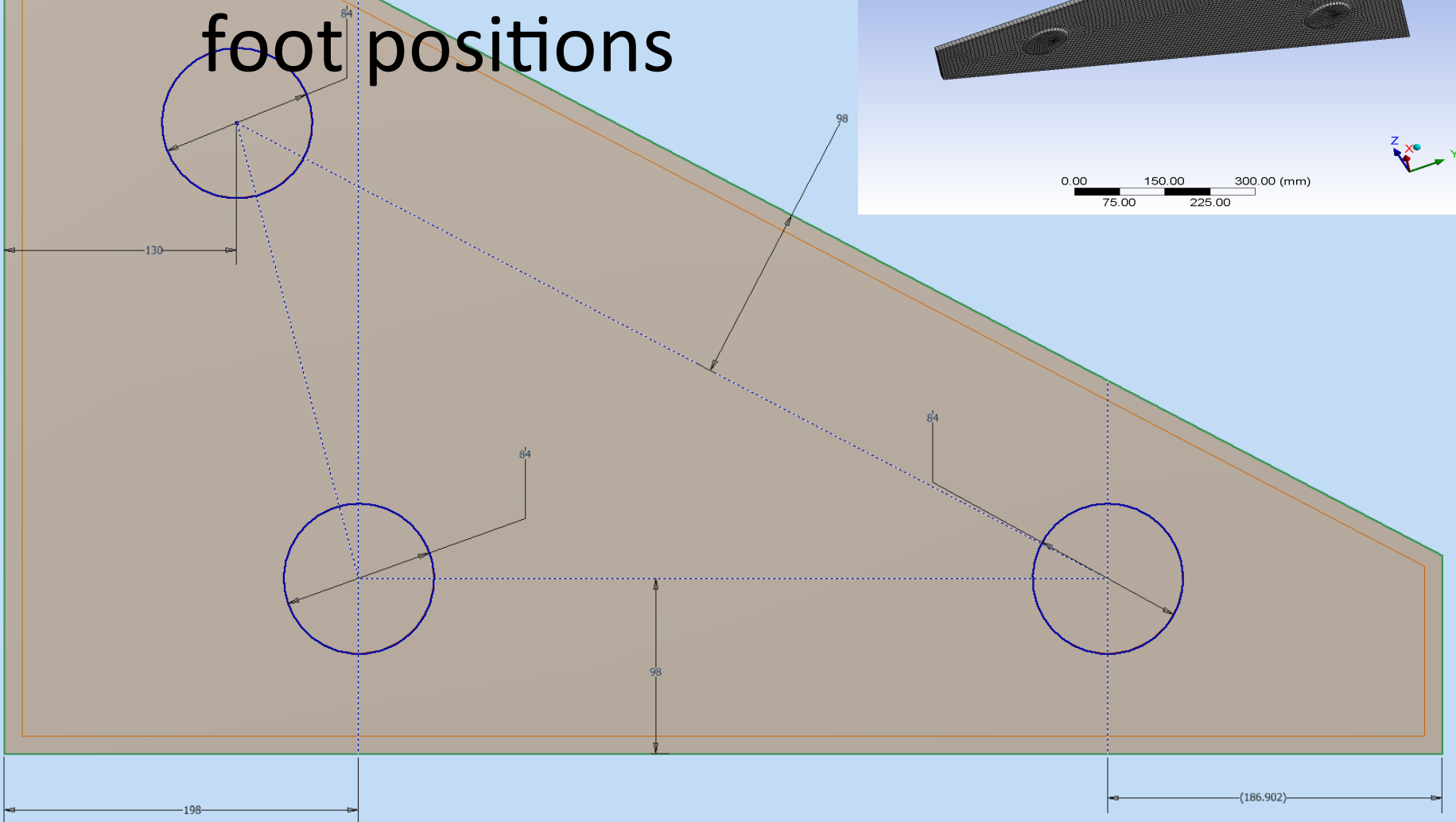
The suggested honeycomb aluminum core is:

Plascore **PCGA-XR1 – 3.1 – 1/8 - .0007 - P - 5052**



4. Polishing of mandrel surface ?

The FEM Model and the optimized foot positions



Aerogel Holding Frame

For the future production the following changes are foreseen:

1. Slightly change of the mirror dimensions
2. Do not insert an Al frame inside the mirror core
3. Glue a 25x35 mm L section bar of 2-3 mm thickness around the mirror perimeter
 - short side on the mirror back
 - long side with machined holes
 - material can be Al or plastic (delrin, MMA, plexiglass, polietilene)
3. Prepare small samples for radiation damage tests

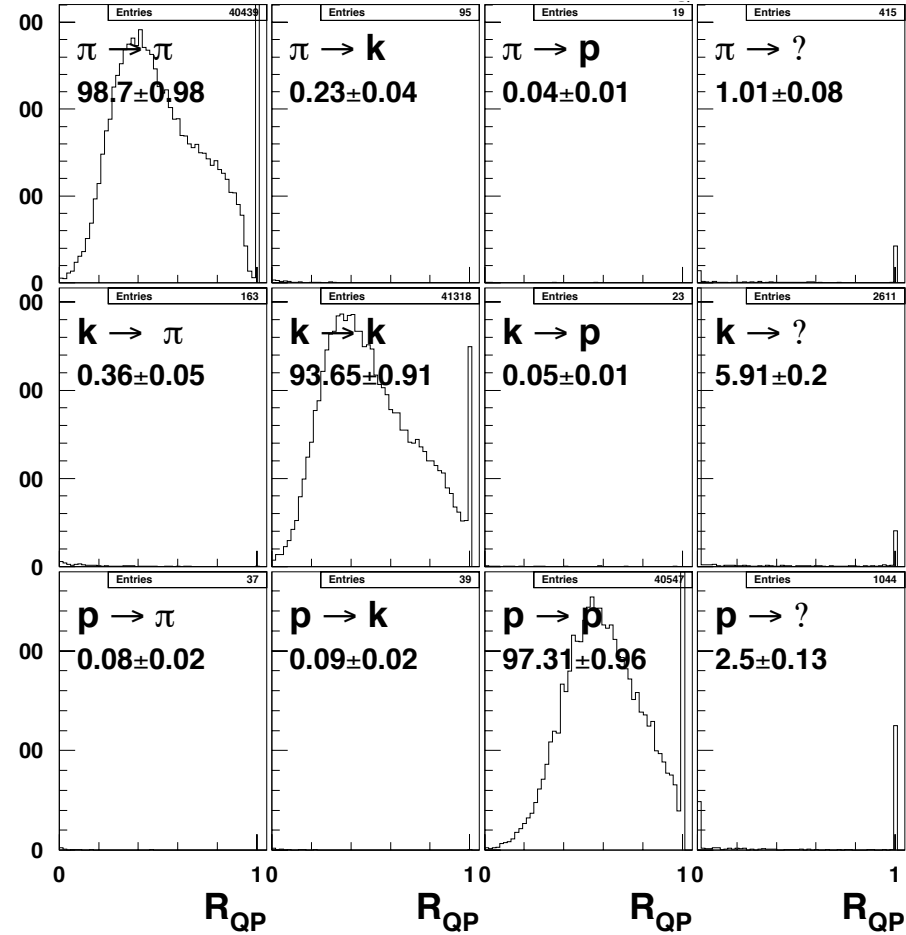
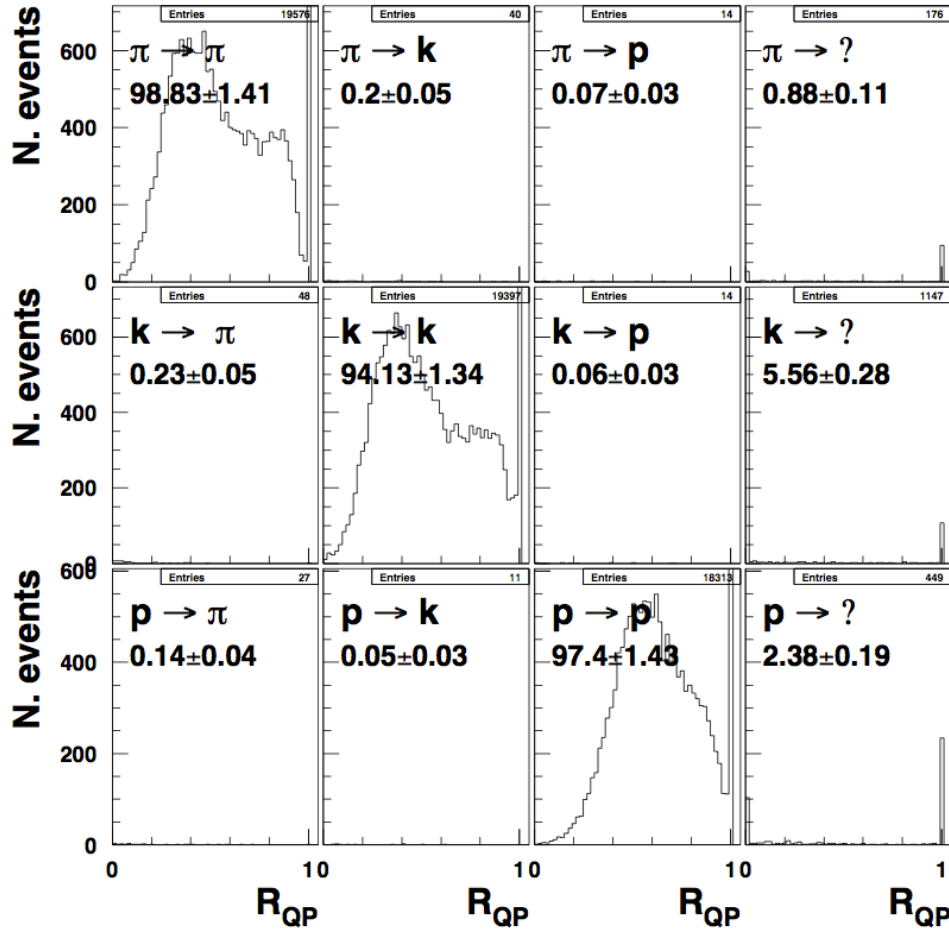
RICH Likelihood

4 m radius mirror

2.7 m radius mirror

$6 \leq E \leq 8$ GeV

$6 \leq E \leq 8$ GeV



RICH Likelihood

4 m radius mirror

2.7 m radius mirror

$3 \leq E \leq 5$ GeV

$3 \leq E \leq 5$ GeV

