

RICH Gas System Design Parameters

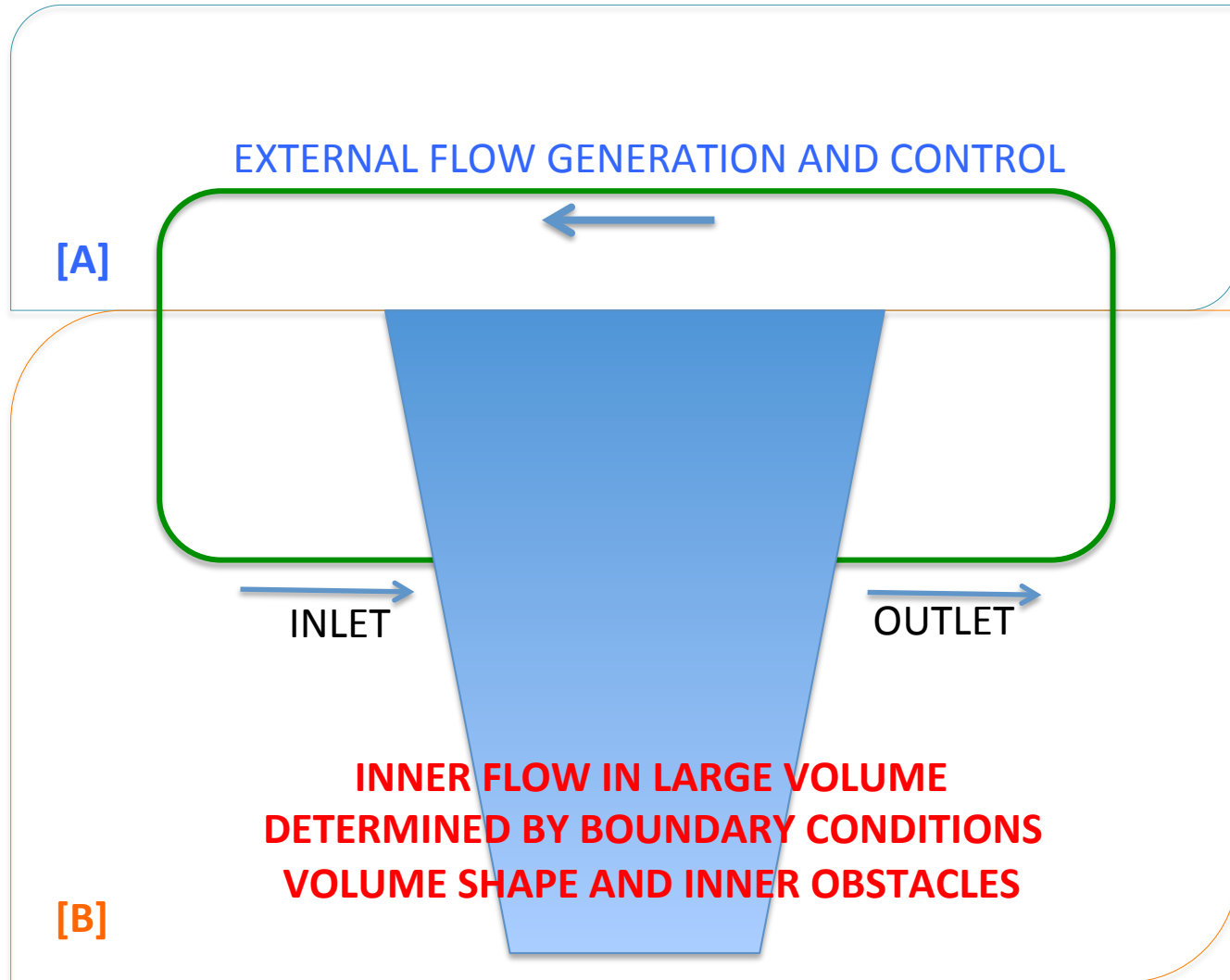
[19.06.2014]

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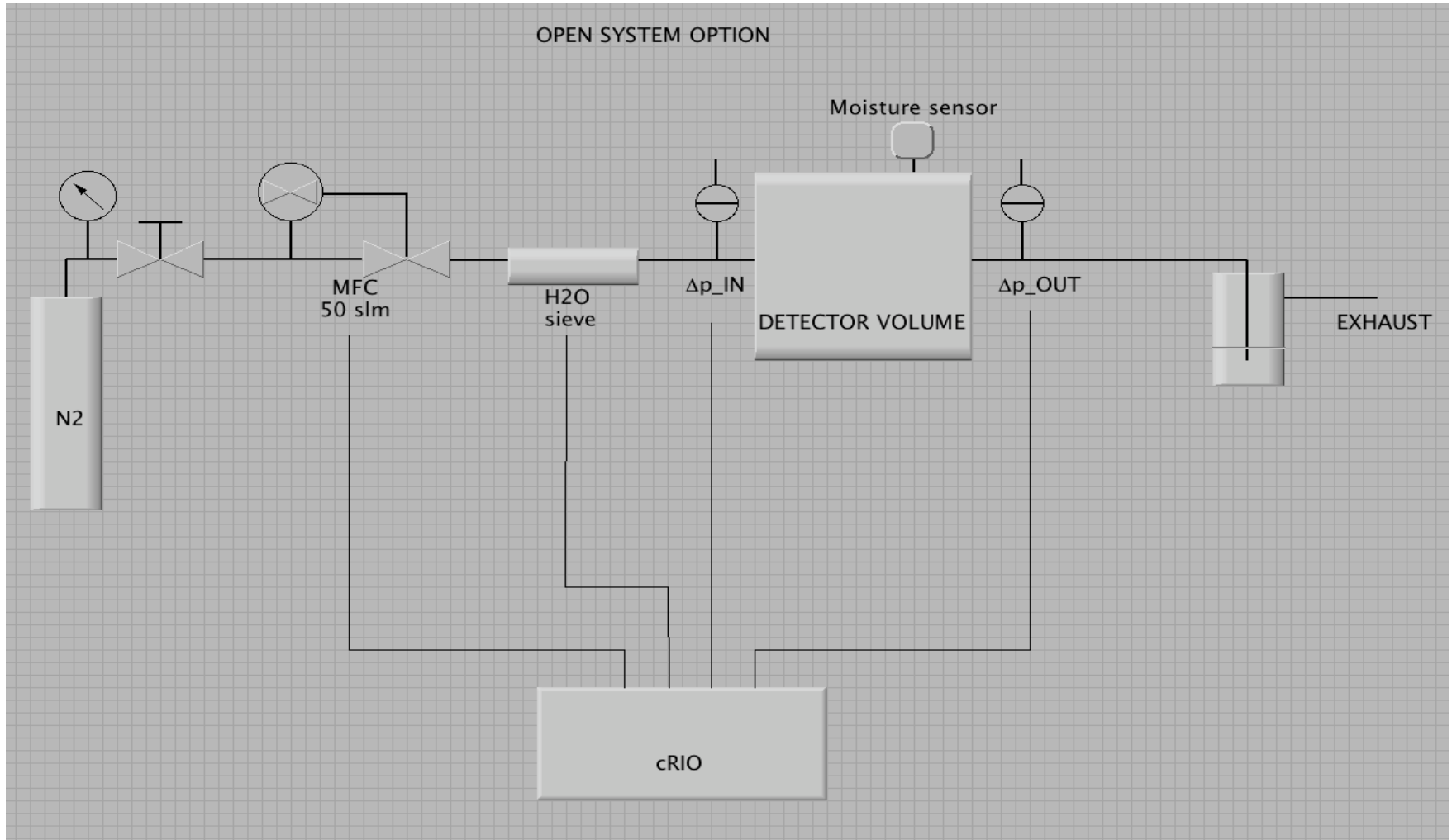
DRY GAS SYSTEM – GENERAL MODEL

[TWO LOGICAL BLOCKS]



DRY GAS SYSTEM BASELINE LAYOUT

[A] FLOW GENERATION AND CONTROL IN OPEN CIRCULATION OPTION



System is flow-driven, i.e. the overpressure is determined by total impedance only. Active controls regulate flow according to overpressure monitors.

DRY GAS SYSTEM BASELINE LAYOUT

requirements:

Volume of interest $\sim 5 \text{ m}^3$

flow:

- dry N2 sufficient to keep H2O concentration below some prefixed level
- 10 nlm ~ 2 volumes/day

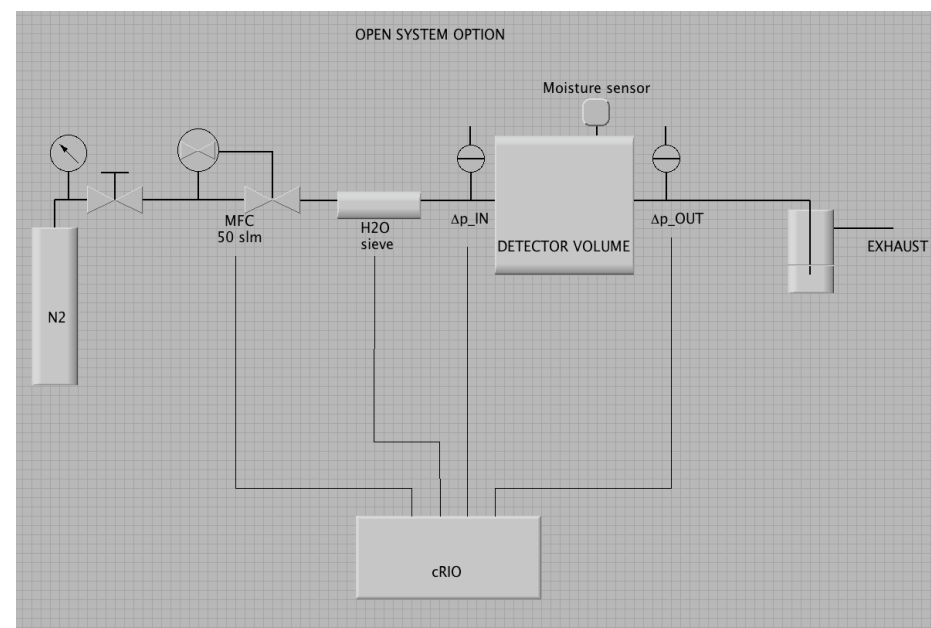
pressure:

wanted levels of $\sim 30\text{-}40$ mbar are not expected to affect mechanics significantly

components:

- [1] MFC e.g. 50 slm F.S.
- [2] single inlets from two sides w/ internal manifolds
- [2] single outlet from one side w/ internal low impedance manifold
- [3] dP for overpressure measurement at chamber inlets and outlets
- [4] H2O sensor(s) at inlets [0-100 PPM]
- [5] Hydrosorb Molecular sieve(s) for H2O filtration

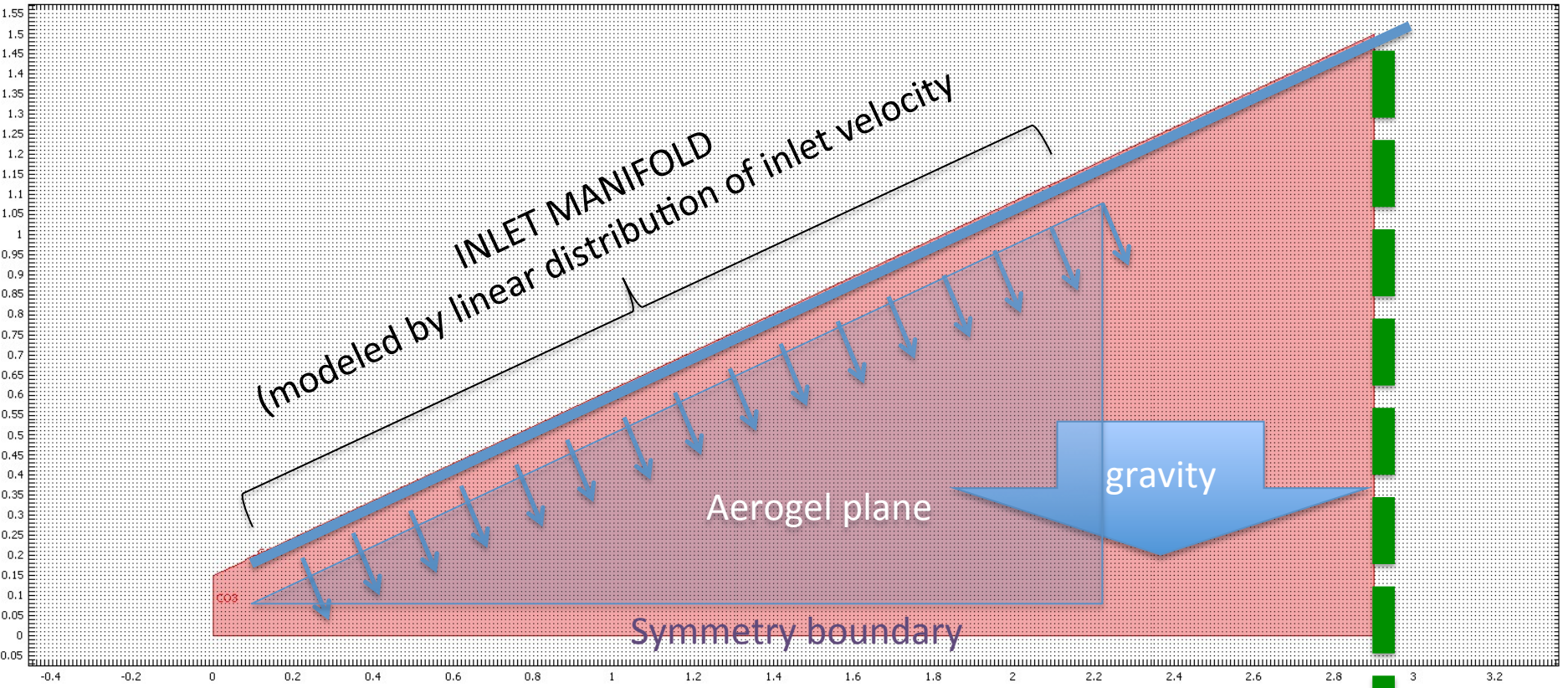
Central controller: e.g. NI-cRIO



2D idealized model: boundary conditions

Concept is that flow is provided by an inlet tube running along the two sides of the front part of the volume in order to flow around the aerogel plane

FRESH DRY N2 FLOW INLET



Outlet manifolds would run along vertical side collecting the flow streamlines to the outside hall (impedances are considered negligible at this stage)

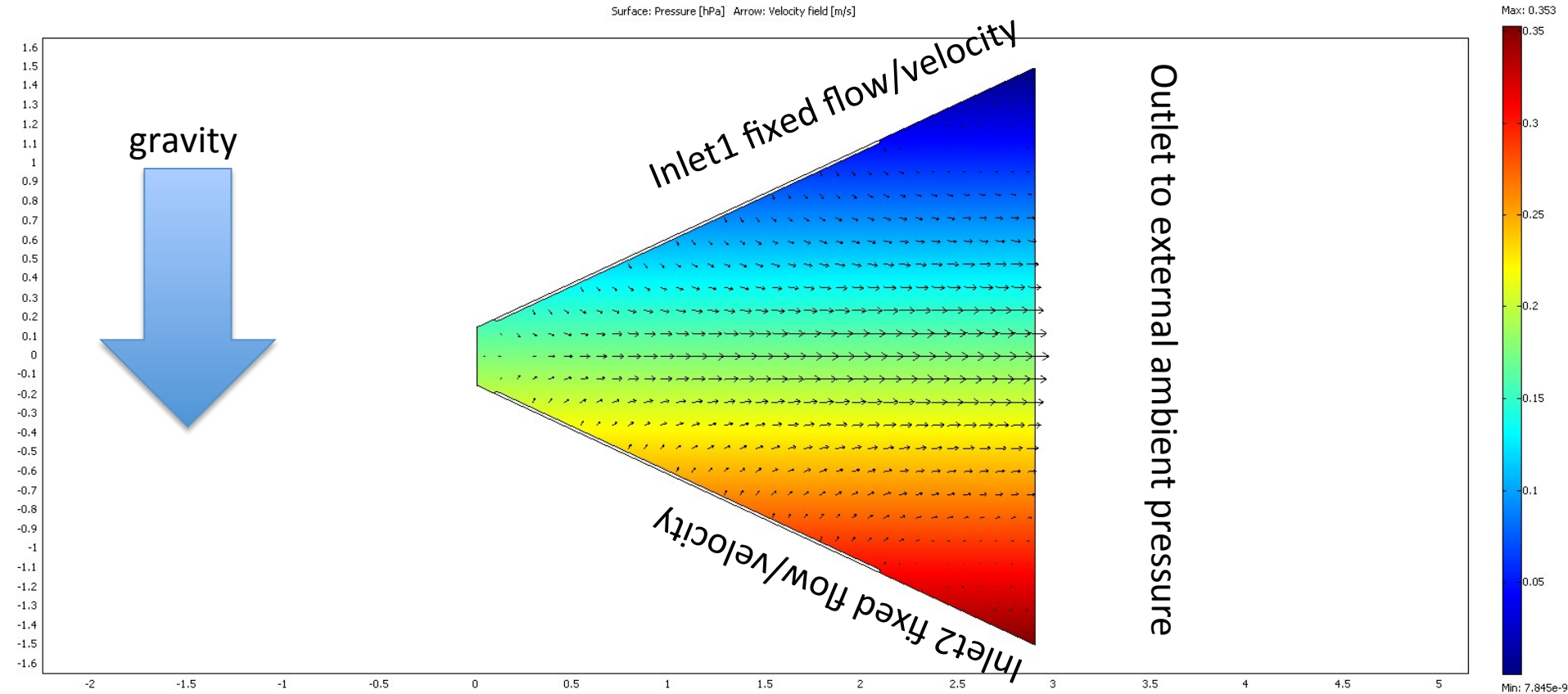
OUTLET MANIFOLD



(modeled by continuous boundary towards outer hydrostatic pressure)

2D idealized model

- > inlets linearly distributed along two sides
- > outlet linearly distributed along one side



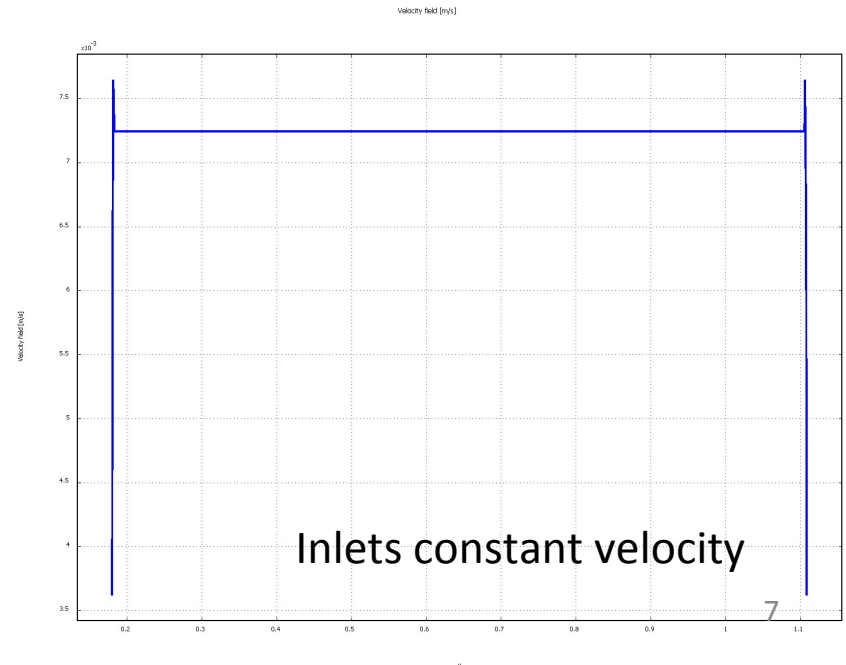
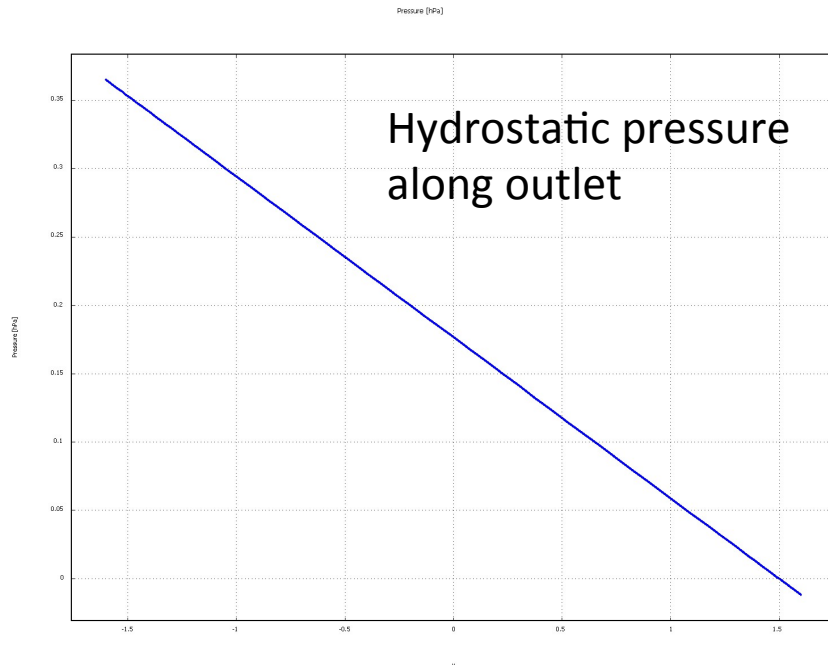
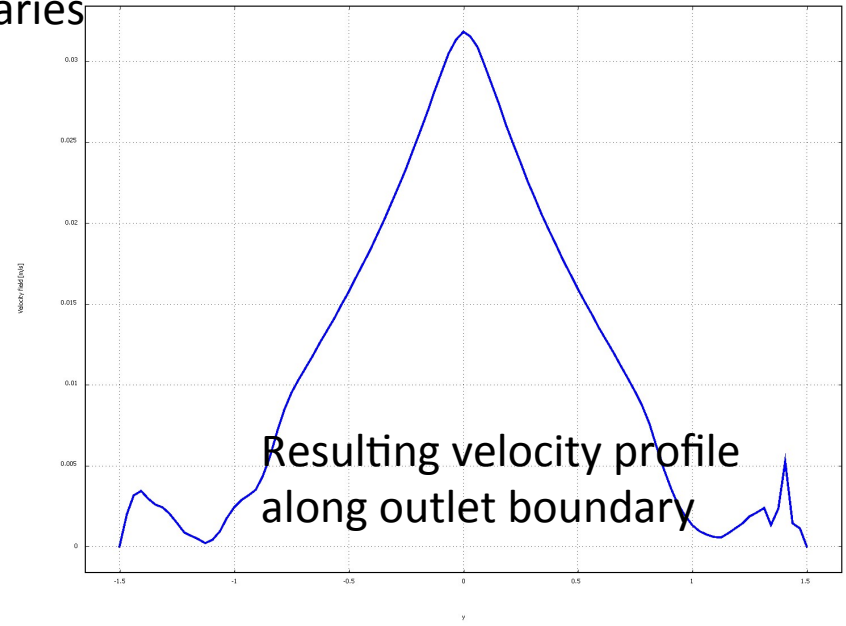
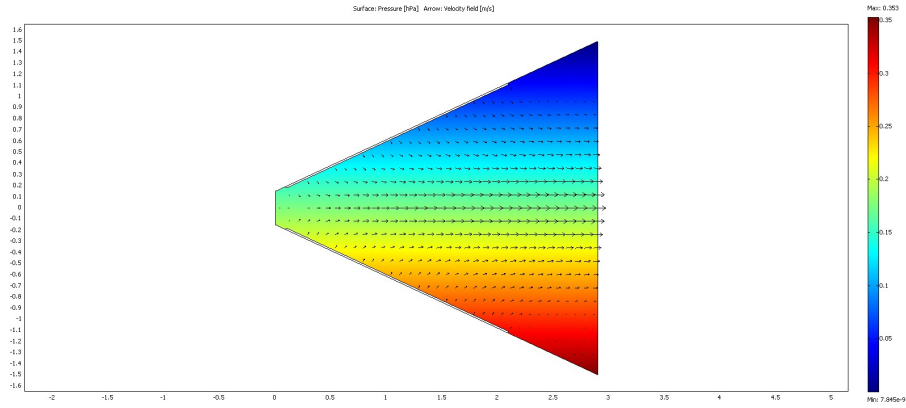
Model is extremely simplified:

inlets are very close to reality (two long inward manifolds)

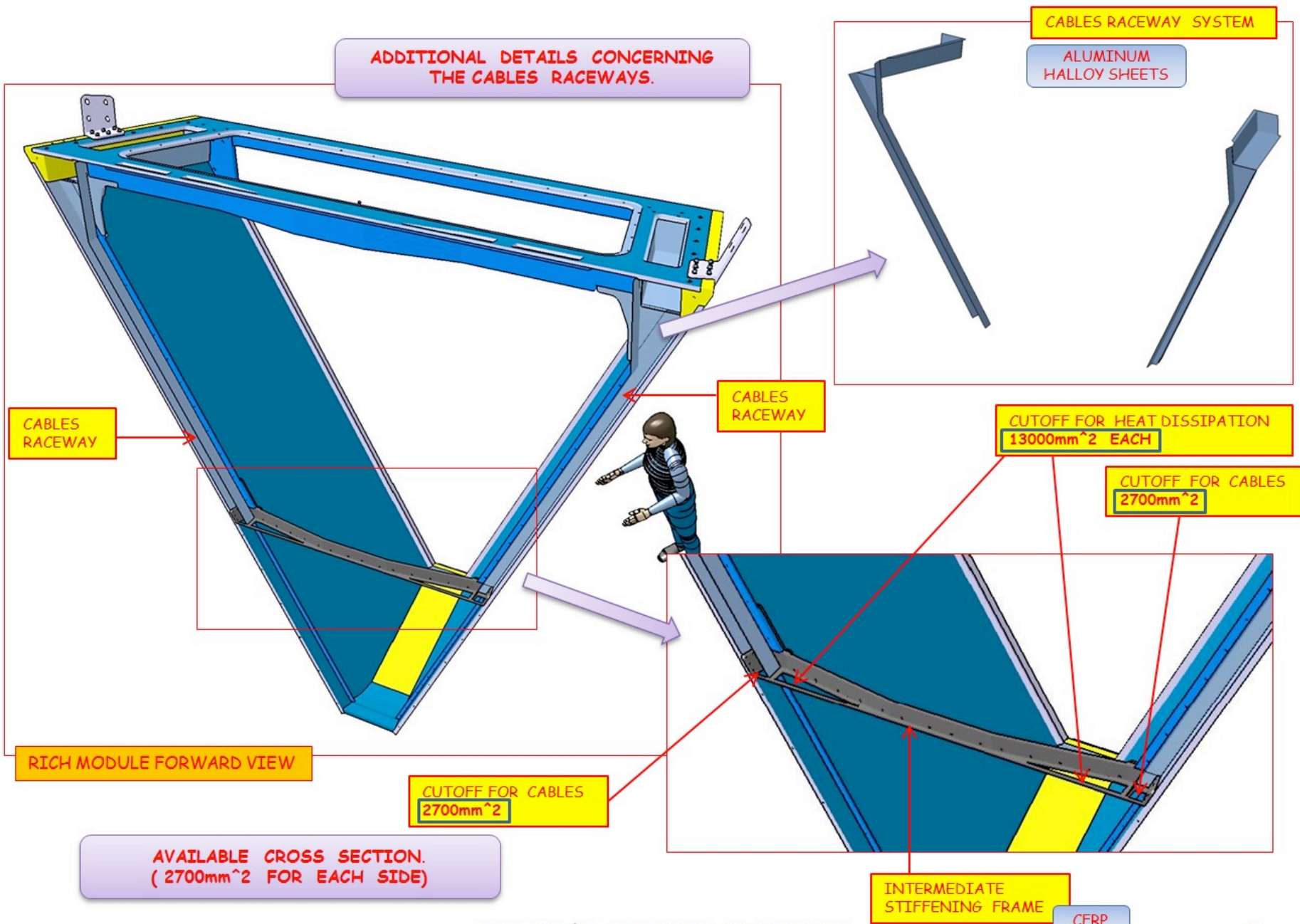
outlet is to be improved with impedance in order to get realistic inner pressure rise

Overall solution features are realistic and ensure expected outward gas flow

Boundary conditions and resulting fields at boundaries



THE RICH Module: Cables Raceways System Details.



THE RICH Module: Cables Raceways System Details.

COOLING OF THE PMT+ELX BOX

Would be possibly an airflow based cooling with forced convection

Access for inlet flow is available from two sides along with the cabling

Removal outlet are also easily available

DETAILS CONCERNING CABLES RACEWAYS.

CABLES RACEWAY SYSTEM

ALUMINUM HALLOY SHEETS

CABLES RACEWAY

CUTOFF FOR HEAT DISSIPATION
13000mm² EACH

CUTOFF FOR CABLES
2700mm²

RICH MODULE FORWARD VIEW

CUTOFF FOR CABLES
2700mm²

AVAILABLE CROSS SECTION.
(2700mm² FOR EACH SIDE)

INTERMEDIATE STIFFENING FRAME

CFRP

Preliminary general physics shows a temperature of ~40 degC would be kept by a steady 5 degC airflow of ~600 nlm

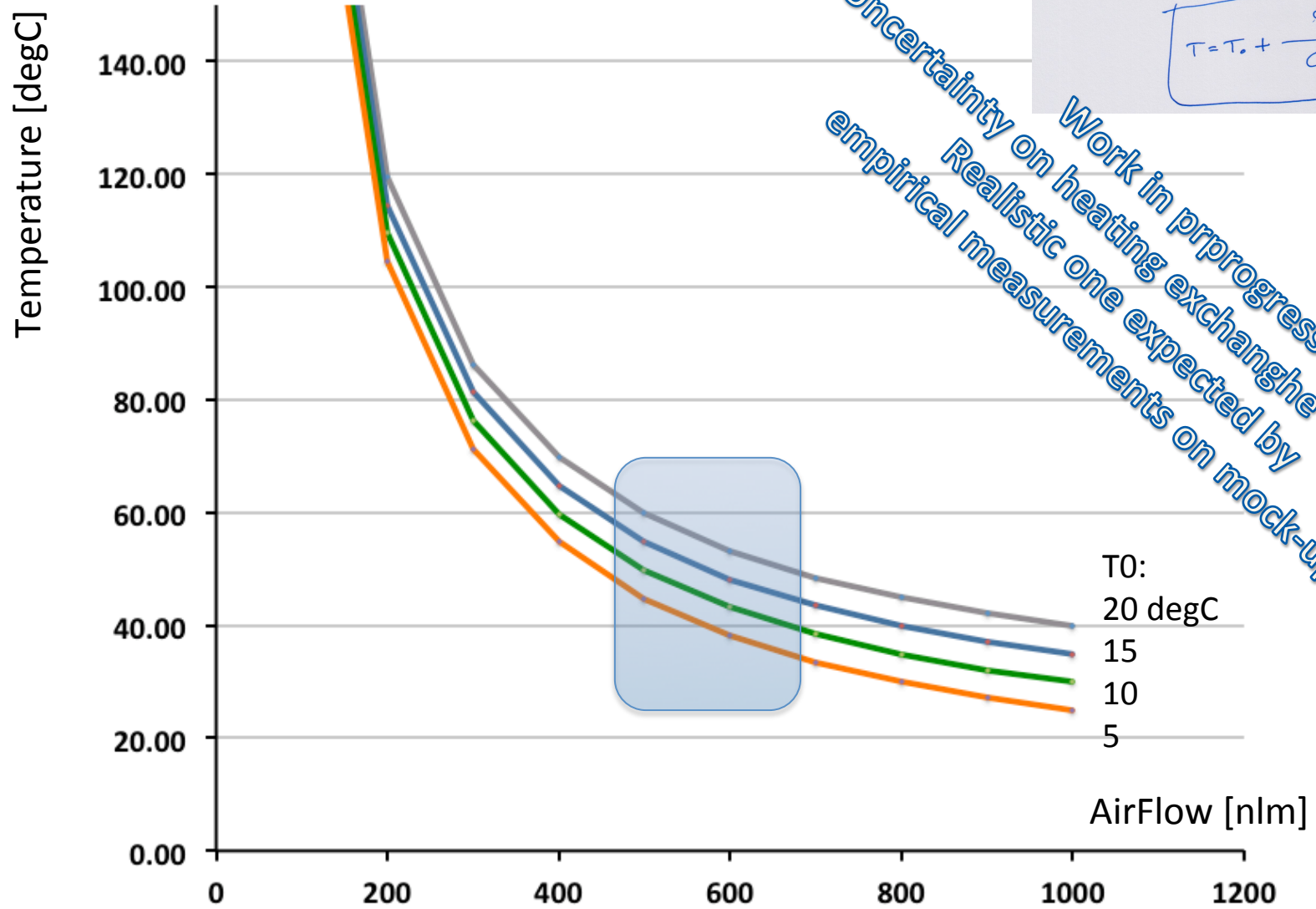
A more relaxed condition of ~60 degC (if acceptable) would be more easily achieved by 20 degC ~500 nlm airflow, certainly avoiding additional technological costs

$$\frac{dQ}{dt} = C_p \frac{dV}{dt} (T - T_0)$$

$$\frac{dQ}{dt} = C_p \frac{dV}{V} \frac{dV}{dt} (T - T_0) = C_p \rho \phi (T - T_0)$$

$$\phi = \frac{dQ/dt}{C_p \rho (T - T_0)}$$

$$T = T_0 + \frac{dQ/dt}{C_p \rho \phi}$$



Uncertainty on heating in progress
 Work in progress
 Realistic one expected by
 empirical measurements on mock-up
 Uncertainty on exchange coefficient

T0:
 20 degC
 15
 10
 5